Designing anisotropy with waveguide subwavelength structures

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ABSTRACT

Silicon sub-wavelength structures have become a versatile design tool for practical, high-performance integrated optical devices, ranging from highly efficient grating couplers to ultra-broadband beam-splitters. Recently, some of the basic anisotropic properties of these structures have been proposed for advance device design. Here we explore these properties in detail, from the underlying physics to emerging applications in on-chip polarization management.

Keywords: subwavelength gratings, anisotropy, homogenization, polarization management

1. INTRODUCTION

Subwavelength grating (SWG) waveguides are segmented with a period (Λ) smaller than the wavelength of light propagating through them [Fig 1(a)], so that diffraction effects are suppressed, and light experiences an equivalent homogenous material. The refractive index of this metamaterial can be varied between the index of the waveguide core and the cladding material by changing the duty cycle (a/Λ) of the structure. This ability to engineer the refractive index is exploited in a variety of high performance silicon photonic devices ranging from low loss fiber-to-chip couplers to compact polarization splitters [1,2]. In most of these applications the SWG is often modelled as an isotropic material. It is, however, well known that such periodic structures are inherently anisotropic [3,4]: essentially light experiences different refractive indexes depending on whether it is polarized parallel (along the x or y axis) or perpendicular (along the z axis) to the grating segments. This interesting property has been exploited only recently. In [5], the use of anisotropic waveguide claddings, which can be implemented with SWGs, was proposed to enhance modal confinement. A multimode interference coupler with ultra-broad bandwidth, exploiting the anisotropy of the SWG to control the propagation constants of higher order modes, was demonstrated in [6]. A similar concept was used to achieve polarization splitting in [7]. Here, we explore how SWGs can be modelled as uniaxial crystals, which provides both valuable physical insight and considerably simplifies the electromagnetic simulation of such structures. More importantly, from the point of view of uniaxial crystals, it becomes clear that rotating the segments, as shown in Fig. 1(b), provides direct control over the anisotropy.

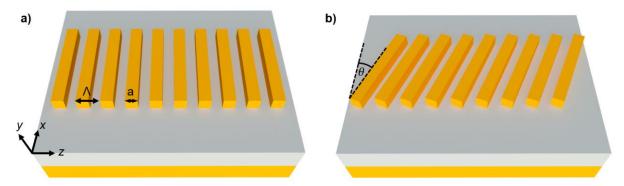


Figure 1. a) In a conventional SWG waveguide light, travelling along the z-direction, experiences a homogenous metamaterial because the pitch of the structure (Λ) is smaller than the wavelength. b) Tilting the waveguide segments with respect to the direction of propagation provides direct control over the anisotropy of the metamaterial.

2. DISCUSSION

The dispersion relation of an infinite laminar medium, composed of two periodically alternating materials, is generally rather complex [8], but, for a period smaller than the wavelength, it is well approximated by that of a uniaxial crystal. We postulate that this approximation continues to hold when to both the infinite width and thickness of the laminar medium are shrunk to the finite dimensions typical for SWG waveguides. From the

dispersion relation in [8], a conventional SWG in silicon on insulator, at a wavelength of $1.55\mu m$, with a period of 200nm and a 50% duty cycle, is described by the tensor

$$n = \begin{bmatrix} n_{xx} = 2.79 & 0 & 0 \\ 0 & n_{yy} = 2.79 & 0 \\ 0 & 0 & n_{77} = 1.94 \end{bmatrix}$$
 (1)

To test the accuracy of this approach we study the propagation through a $3\mu m$ wide SWG waveguide ($\theta = 0^{\circ}$) using both 3D FDTD simulations of the segmented structure, and simple modal analysis of the equivalent uniaxial crystal. As shown in Table 1, the field plots resulting from the 3D FDTD simulations and the model are virtually indistinguishable, for both polarizations, and the relative error in the effective index (n_{eff}) is below 3%.

Table 1. Field propagation through SWG waveguides computed with 3D FDTD and modal analysis of the corresponding crystal.

θ	TE (polarized in x-z plane)		TM (polarized along the y axis)	
	3D FDTD	Anisotropic Model	3D FDTD	Anisotropic Model
0°	$\Re\{E_x(x,z)\}$	$\Re\{E_x(x,z)\}$	$\Re\{E_y(x,z)\}$	$\Re\{E_y(x,z)\}$
	2 0 -2 (mt/) sixe-x	2 0 2 (un/) sixe-x	(mt/) sixe-x -2	2 0 -2 -2
	0 1 2 z-axis (μm)	0 1 2 z-axis (μ m)	0 1 2 z-axis (μ m)	0 1 2 z-axis (μ m)
				1
-	$n_{eff} = 2.13$	$n_{eff} = 2.17$	$n_{eff} = 1.60$	$n_{eff} = 1.61$
30°	$\Re\{E_x(x,z)\}$	$\Re\{E_x(x,z)\}$	$\Re\{E_y(x,z)\}$	$\Re\{E_y(x,z)\}$
	(m <i>t</i>) sixe-x	(mt/) sixe-x	(mt) sixe-x -2	2 0 -2 -2
	0 1 2	0 1 2	0 1 2	0 1 2
	z-axis (μ m)	z-axis (μ m)	z-axis (μ m)	z-axis (μ m)
	$n_{eff} = 2.00$	$n_{eff} = 2.04$	$n_{eff} = 1.62$	$n_{eff} = 1.63$

Tilting the SWG segments as shown in Fig. 1(b) is clearly equivalent to a rotation of the crystal, i.e. the tensor in Eq. (1) will be rotated by the angle θ [9]. Since this rotation leaves the n_{yy} component of the tensor in Eq. (1) constant, one may expect that the TM modes, which are polarized along the y axis, will be mostly unaffected, whereas the TE modes will change. This is observed in the simulations results shown in Table 1 for $\theta = 30^\circ$, thereby confirming that tilting of the SWG segments provides direct control over the anisotropy of the equivalent metamaterial.

We apply this technique to design the high-performance polarization splitter shown in Fig. 2. The device is based on a multimode interference coupler, where the beat-length for TE polarization is half the beat-length for TM polarization. As a result, the devices images a TE polarized input from port 1 to the upper output (port 2), whereas a TM polarized input is imaged to the lower output (port 3).

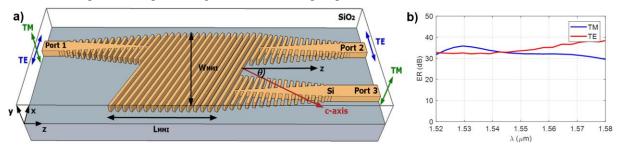


Figure 2. a) By tilting the SWG segments, this multi-mode interference polarization splitter can be independently optimized for TE and TM polarization. b) 3D FDTD simulations of the device reveal virtually wavelength independent extinction ratios, in excess of 30dB, for both polarizations.

By using this strategy, we were able to adjust the beat-lengths for both polarizations simply by changing the tilting angle of the structure to ~12°, so the remaining geometric parameters could be used to optimize the performance of the device. As shown in Fig. 2(b), 3D FDTD simulations of the complete structure show that this results in very high extinction ratios for both polarizations, that remain virtually constant over the complete C band

3. CONCLUSIONS

We have proposed and validated a model, based on uniaxial crystals, that represents the intrinsic anisotropy of SWG waveguides. We have furthermore shown that that tilting the SWG segments provides control over the anisotropy of structures, as predicted by the model. This new degree of freedom can be used to design high performance integrated polarization management devices.

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